

Determination of Second Virial Coefficients and Virial Equations of R-32 (Difluoromethane) and R-125 (Pentafluoroethane) Based on Speed-of-Sound Measurements¹

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The second virial coefficients, B , for difluoromethane (R-32, CH_2F_2) and pentafluoroethane (R-125, CF_3CHF_2) are derived from speed-of-sound data measured at temperatures from 273 to 343 K with an experimental uncertainty of $\pm 0.0072\%$. Equations for the second virial coefficients were established, which are valid in the extensive temperature ranges from 200 to 400 K and from 240 to 440 K for R-32 and R-125, respectively. The equations were compared with theoretically derived second virial coefficient values by Yokozeki. A truncated virial equation of state was developed using the determined equation for the virial coefficients. The virial equation of state represents our speed-of-sound data and most of the vapor $P\rho T$ data measured by deVries and Tillner-Roth within ± 0.01 and $\pm 0.1\%$, respectively.

KEY WORDS: alternative refrigerant; equation of state; hydrofluorocarbon; R-32; R-125; second virial coefficient; speed of sound.

1. INTRODUCTION

Since the speed of sound in the dilute gas depends heavily on the ideal-gas heat capacity, the second virial coefficients can be accurately determined from speed-of-sound measurements. Hydrofluorocarbons, R-32, R-125, and

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1,1,1,2-tetrafluoroethane (R-134a, CH_2FCF_3) are components of promising binary and/or ternary refrigerant mixtures to replace chlorodifluoromethane (R-22, CHClF_2). The speed of sound in gaseous R-32 [1, 2], R-125 [3], and R-134a [2, 4] has been measured with an uncertainty of $\pm 0.0072\%$.

The second virial coefficient is important to calculate thermodynamic properties at low temperatures and low pressures where experimental data are scarce. The virial coefficients for R-134a were determined recently [5, 6] by a new analytical method. In the present study, second virial coefficients are determined from this new analytical method based on experimental speed-of-sound values for R-32 and R-125. The determined values are compared with literature results. A simple virial equation of state is also developed based on the determined values. The experimental speed-of-sound and $P\rho T$ data are compared with calculated values from the equations of state.

2. DETERMINATION OF SECOND VIRIAL COEFFICIENTS FROM SPEED OF SOUND

Since a detailed explanation of the use of speed-of-sound measurements for the determination of second virial coefficients has been presented in previous papers [5, 6], only a brief explanation is given here. The speed-of-sound data were measured at various temperatures and pressures; however, the density was not measured. The second virial coefficients of the density-series virial equation are useful in the development of equations of state. The virial coefficients, B' , C' , D' , and E' , of a pressure-series virial equation (denoted by a prime) are related to the virial coefficients, B , C , and D of a density-series virial equation as follows:

$$B' = \frac{B}{RT} \quad (1)$$

$$C' = \frac{C - B^2}{(RT)^2} \quad (2)$$

$$D' = \frac{D + 2B^3 - 3BC}{(RT)^3} \quad (3)$$

$$E' = \frac{E - 5B^4 + 10B^2C - 4BD - 2C^2}{(RT)^4} \quad (4)$$

By using Eqs. (1)–(4), a pressure-series virial equation with the virial coefficients of a density-series virial equation is derived as expressed by Eq. (5).

$$Z = 1 + \frac{B}{RT} P + \frac{C - B^2}{(RT)^2} P^2 + \frac{D + 2B^3 - 3BC}{(RT)^3} P^3 + \frac{E - 5B^4 + 10B^2C - 4BD - 2C^2}{(RT)^4} P^4 \quad (5)$$

The Gibbs function is derived from Eq. (5) using ideal-gas heat capacities [2, 3], and the speed of sound is derived from the Gibbs function by using a general thermodynamic relation. The virial coefficients of a density-series virial equation can be derived by fitting the equation to the experimental speed-of-sound data with temperature and pressure values.

Before carrying out the procedure discussed above, we examined the number of terms of virial equations needed for representing the $P\rho T$ properties over the same range of the speed-of-sound data [1-3]. For almost the entire range of the gaseous phase, only a two-term density-series virial equation with the second and third virial coefficients is needed for the required accuracy, whereas a four-term pressure-series virial equation with the second to fifth virial coefficients is needed to represent the $P\rho T$ properties over the same range of the present speed-of-sound data with the same deviations as those of the density-series virial equation. The number of terms are the same for R-32, R-125, and R-134a.

We fitted Eq. (5), with the fourth and fifth virial coefficients of the density-series virial equation being zero ($D = 0$ and $E = 0$), to the speed-of-sound measurements, and then we determined the second and third virial coefficients. Because the fitting range is a very small region of the dilute gaseous phase, it is not possible to determine the third virial coefficient from the present speed-of-sound measurements. When we fitted Eq. (5) to the speed-of-sound measurements, we used the following temperature function:

$$B = b_0 + b_1 \exp\left(\frac{b_2}{T}\right) \quad (6)$$

The determined coefficients of Eq. (6) are presented in Table I for both R-32 and R-125.

Table I. Coefficients of Eq. (6) for R-32 and R-125

	R-32	R-125
b_0 ($\text{cm}^3 \cdot \text{mol}^{-1}$)	75.183	194.42
b_1 ($\text{cm}^3 \cdot \text{mol}^{-1}$)	-40.088	-109.405
b_2 (K)	667.86	489.41

Table II. Coefficients of Eq. (8) for R-32 and R-125

	R-32	R-125
c_1 (dm ⁶ ·mol ⁻²)	2.357×10^{-2}	1.107×10^{-2}
c_2 (K)	310.94	489.41
c_3 (dm ⁶ ·mol ⁻²)	-1.50×10^{-4}	-1.46×10^{-5}
α	3.354	2.426
β	16.41	13.27

3. FORMULATION OF VIRIAL EQUATION OF STATE

A simple truncated virial equation of state is formulated by simply assigning functional forms to B and C .

$$Z = 1 + B\rho + C\rho^2 \quad (7)$$

The functional form for B is Eq. (6), and the coefficients of b_0 , b_1 , and b_2 are determined from the experimental speed-of-sound values. Since the contribution of C to the speed of sound at low pressure is very small, the C values are determined based on available experimental $P\rho T$ values [7, 8].

The functional form of C is taken as

$$C = c_1 \left(\frac{c_2}{T} \right)^\alpha + c_3 \left(\frac{c_2}{T} \right)^\beta \quad (8)$$

where c_1 , c_2 , c_3 , α , and β are fitting parameters. Namely, the present virial equation of state, Eq. (7), consists of four temperature and density terms as shown in Eqs. (6) and (8).

The C values were determined with accurate experimental $P\rho T$ values by fitting the coefficients in Eq. (8). For the determination of the four-term virial equations of state, the experimental $P\rho T$ values of R-32 and R-125 reported by Zhang et al. [7] and by de Vries and Tillner-Roth [8] were used. The determined parameters in Eq. (8) are given in Table II for R-32 and R-125, while the ranges of validity of Eq. (7) for R-32 and R-125 are reported in Table III. The ranges include most of the gaseous phase region

Table III. Range of Eq. (7) for R-32 and R-125

	T (K)	P (MPa)	ρ (kg·m ⁻³)
R-32	263–383	0–6.0	0–150
R-125	263–390	0–4.0	0–300

for these refrigerants. The present four-term virial equation can be used for prediction of thermodynamic properties at very low temperatures because of the reasonable behavior of the second virial coefficients as shown in Figs. 1 and 2 and explained in the following section.

4. RESULTS AND DISCUSSION

4.1. Second Virial Coefficients

The experimental speed-of-sound data at constant temperature are fitted by a quadratic speed-of-sound equation of the pressure series type, but the speed-of-sound data should be fitted by a more complicated equation as derived from Eq. (5). Figures 1 and 2 show the differences between the second virial coefficient derived by a previous method [1–4] and those by the present procedure for R-32 and R-125, respectively.

Figure 1 shows comparisons of the second virial coefficient for R-32. The values of Zhang et al. [9] and de Vries and Tillner-Roth [8] for R-32 agree with results from Eq. (6) within ± 0.6 and $\pm 1.8\%$, respectively. We plotted the theoretical values of Yokozeki et al. [10], which agree with the present results within $\pm 2.0\%$, even at temperatures below 260 K and above 380 K. The previous values [1] agree with present results within $\pm 2.0\%$ over a limited temperature range, 273 to 343 K. However, the extrapolated second virials of the previous paper [1] deviate by -15% from the present values at 200 K. Since the thermodynamic state of R-32 is much closer to the ideal-gas condition than that of R-125, the second virial coefficient of R-32 is more difficult to be determined from experimental results.

For R-125, the second virials of Zhang et al. [9], Gillis [11], and Boyes and Weber [12] agree with calculated values from Eq. (6) within ± 1.7 , ± 2.4 , and $\pm 0.7\%$, respectively, as shown in Fig. 2. The theoretical values of Yokozeki et al. [10] agree well with the present results, i.e., within $\pm 0.6\%$ over the range of validity of the present model. Even if Eq. (6) is extrapolated to temperatures below 260 K and to temperatures above 390 K, the present second virials agree with those of Yokozeki et al. [10] within $\pm 3.0\%$. And we also show in Fig. 2 the previous second virials [3], which have been determined by using second acoustic virial coefficients. The previous values [3] agree with present values within $\pm 1.6\%$ from 240 to 440 K since the contribution of the second virials to the speed of sound is sufficiently large to allow accurate calculations of the second virials.

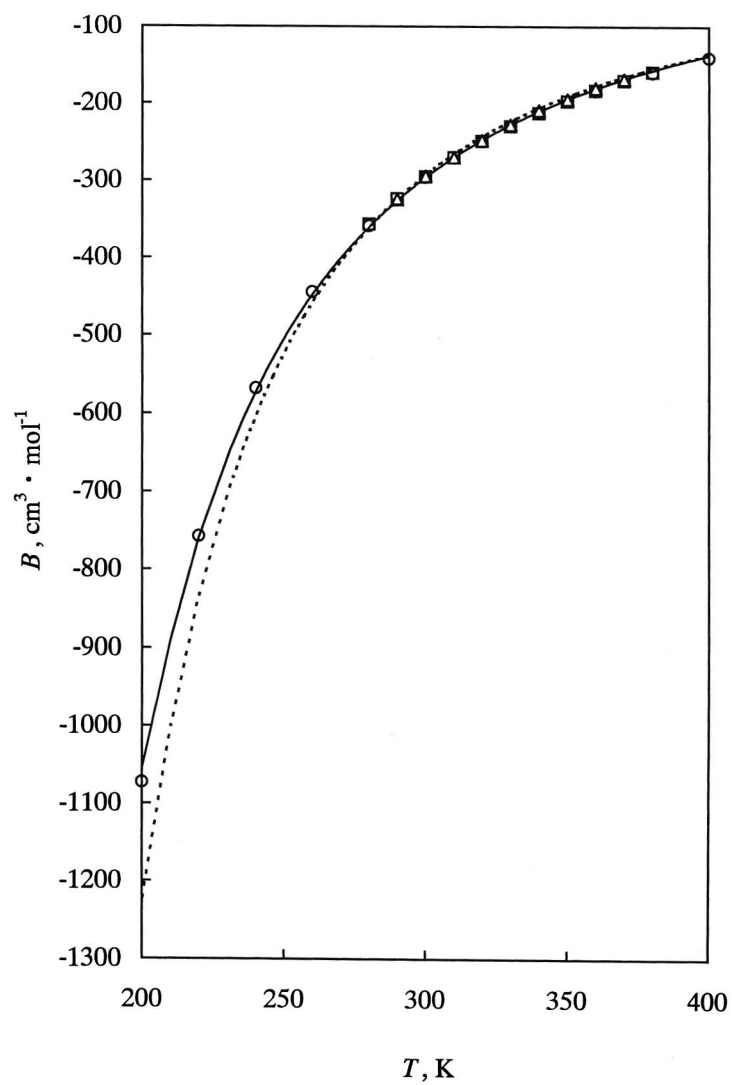


Fig. 1. Second virial coefficients for R-32. (Δ) Zhang et al. [9]; (\square) de Vries and Tillner-Roth [8]; (\circ) Yokozeki et al. [10]; (- - -) Hozumi et al. [1]; (—) calculated values from Eq. (6).

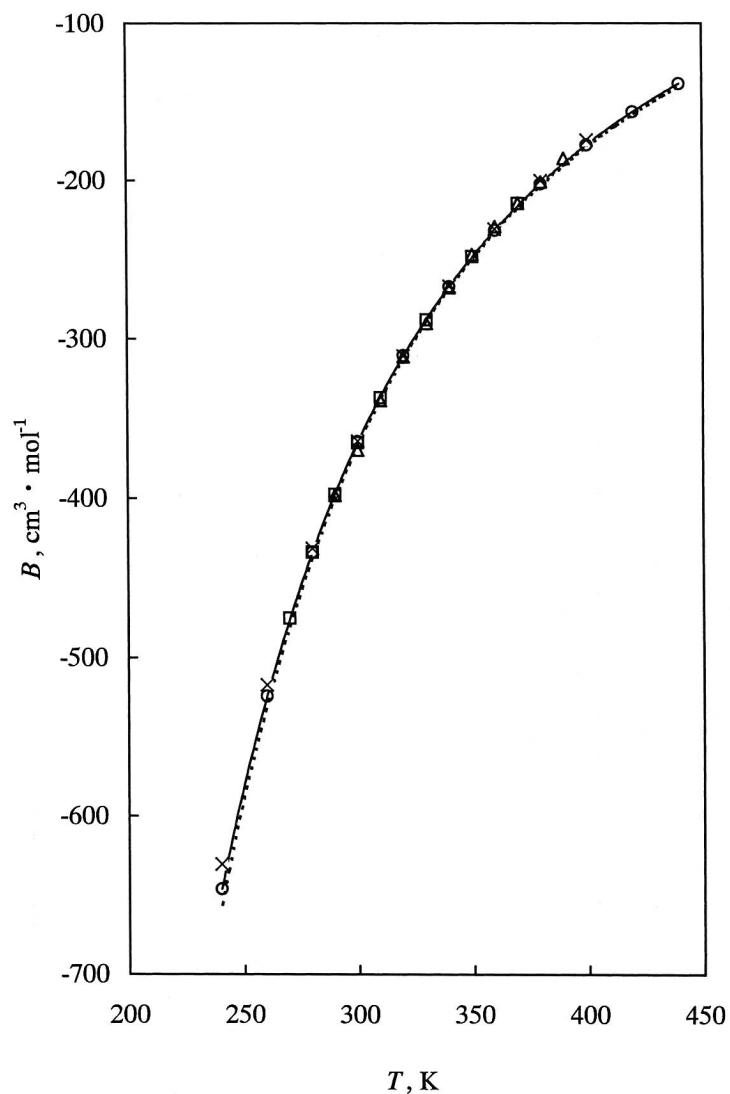


Fig. 2. Second virial coefficients for R-125. (Δ) Zhang et al. [9]; (\times) Gillis [11]; (\square) Boyes and Weber [12]; (\circ) Yokozeki et al. [10]; (---) Hozumi et al. [3]; (—) calculated values from Eq. (6).

4.2. Virial Equation of State

Figures 3 and 4 show the deviations of the experimental speed-of-sound data from the calculated values using the four-term virial equations of state for R-32 and R-125, respectively. For R-32, the speed-of-sound data [1, 2] agree well within $\pm 0.006\%$ with the calculated values from Eq. (5), as shown in Fig. 3. The experimental speed-of-sound data [3] for R-125 agree with the calculated values from Eq. (5) within $\pm 0.011\%$ as shown in Fig. 4.

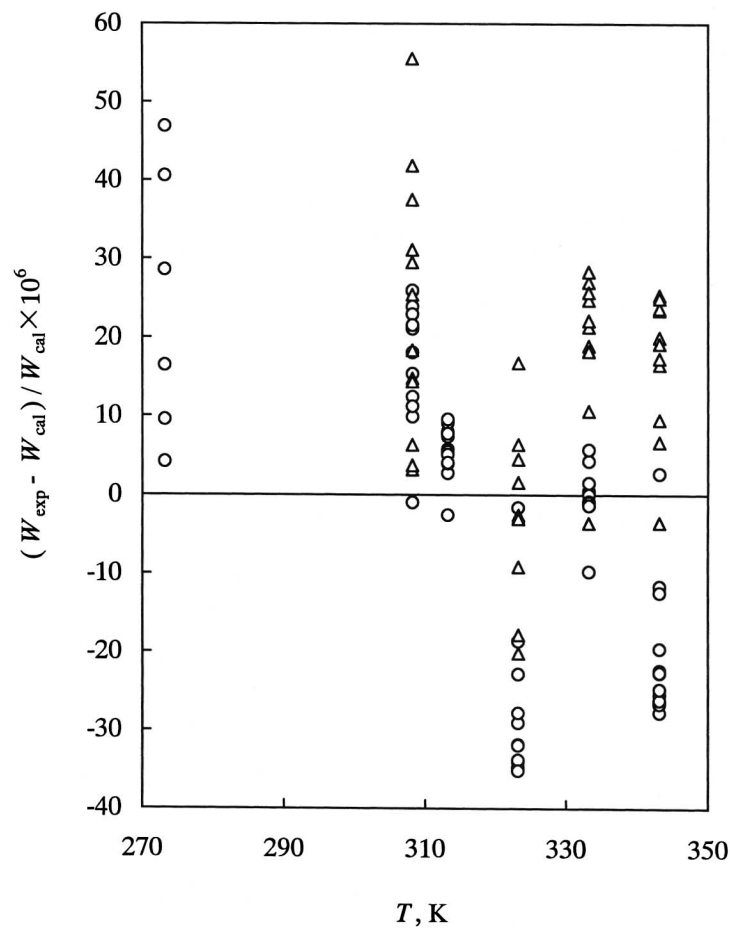


Fig. 3. Deviations of experimental speeds of sound from calculated values of Eq. (5) for R-32. (○) Hozumi et al. [1]; (△) Hozumi et al. [2]; (—) calculated values from Eq. (5).

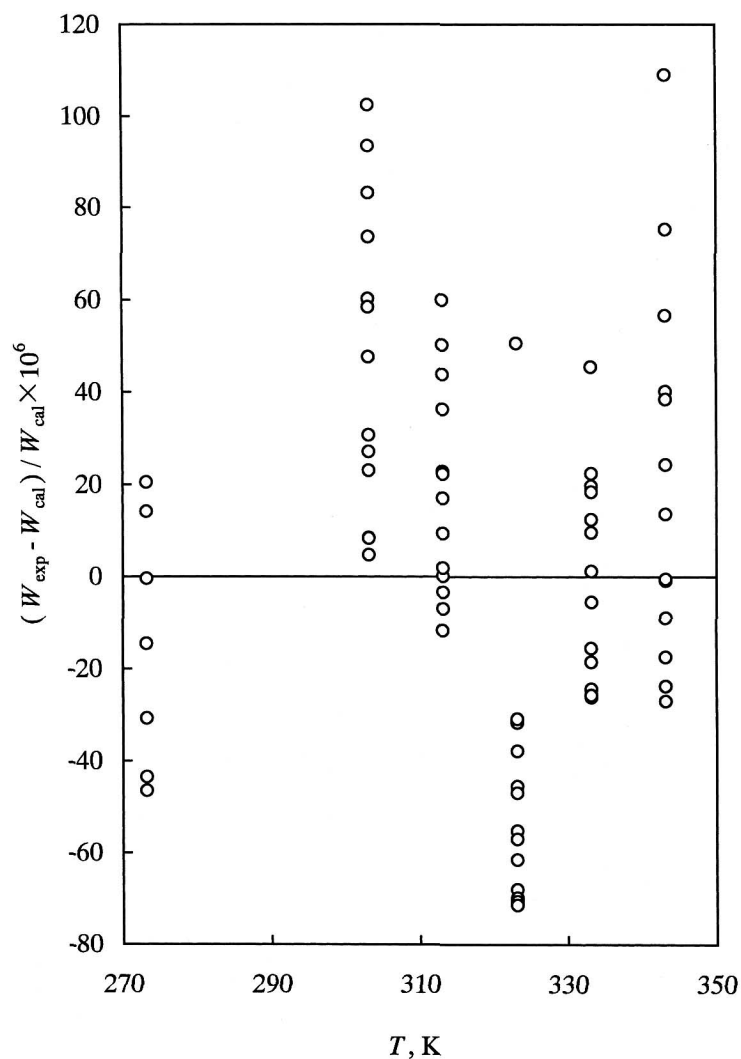


Fig. 4. Deviation of experimental speeds of sound from calculated values of Eq. (5) for R-125. (○) Hozumi et al. [3]; (—) calculated values from Eq. (5).

The deviations of experimental $P\rho T$ data from the present four-term virial equation of state are shown in Figs. 5 and 6. In Fig. 5, the experimental $P\rho T$ data reported by Zhang et al. [7] and by de Vries and Tillner-Roth [8] for R-32 agree with the calculated values from Eq. (7) within $\pm 0.1\%$ in pressure. In Fig. 6 the experimental $P\rho T$ data reported by de Vries and

Tillner-Roth [8] for R-125 agree very well with the calculated values from Eq. (7), within $\pm 0.05\%$ in pressure. On the other hand, the data reported by Zhang et al. [7] for R-125 agree with the calculated values from Eq. (7) within $\pm 0.20\%$ except for four data points at higher densities along the 290, 320, and 390 K isotherms.

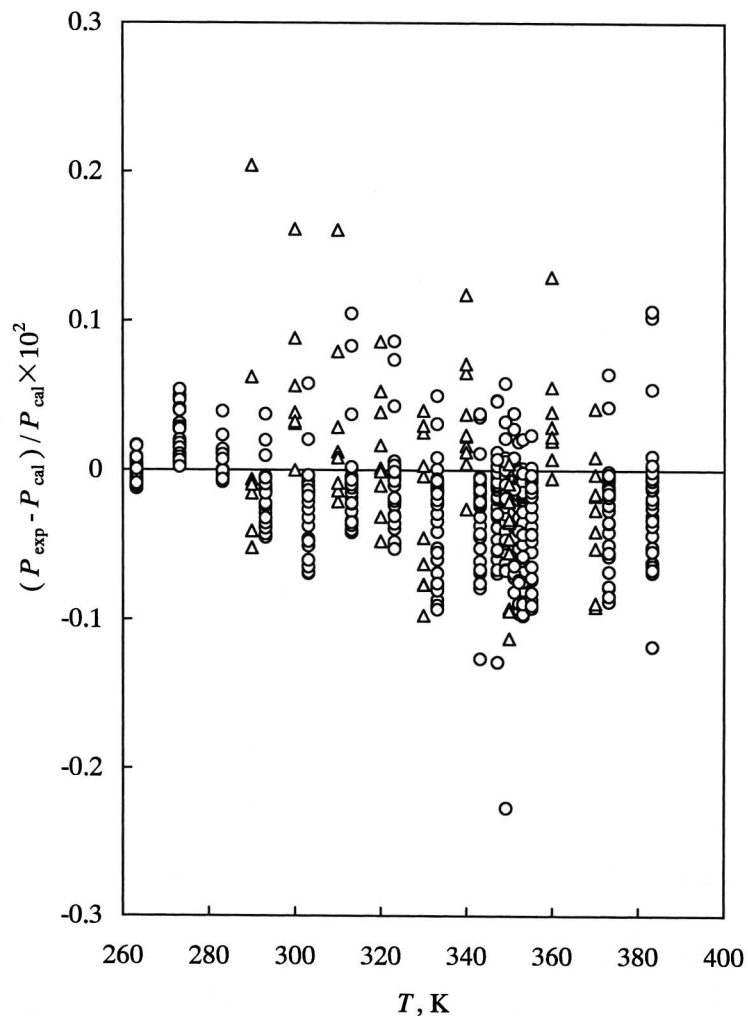


Fig. 5. Deviation of experimental PpT data from calculated values of Eq. (7) for R-32. (Δ) Zhang et al. [7]; (\circ) de Vries and Tillner-Roth [8]; (—) calculated values from Eq. (7).

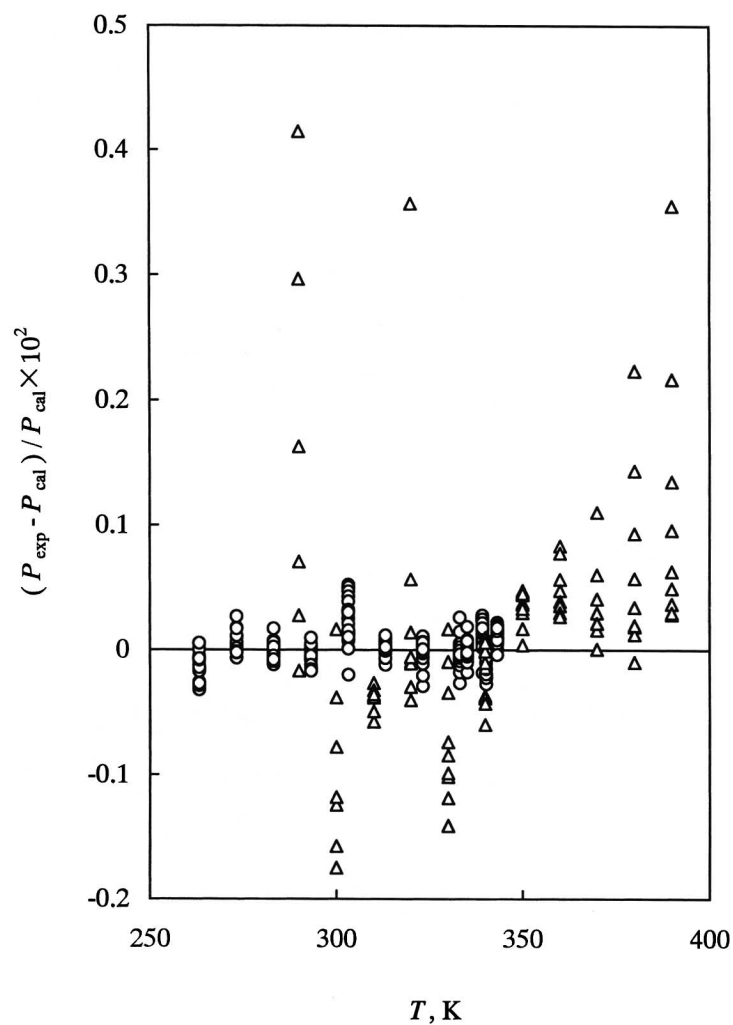


Fig. 6. Deviation of experimental $P\rho T$ data from calculated values of Eq. (7) for R-125. (Δ) Zhang et al. [7]; (\circ) de Vries and Tillner-Roth [8]; ($—$) calculated values from Eq. (7).

5. CONCLUSIONS

We determined the second virial coefficients from the experimental speed-of-sound data for R-32 and R-125 using a new method. The determined second virial coefficients agree well with the reported experimental data. The second virials for R-32 and R-125 agree well with theoretical

values, even at temperatures far beyond the range of the speed-of-sound measurements, the temperature range is 200 to 400 K for R-32 and 240 to 440 K for R-125. The present four-term virial equation of state represents experimental speed-of-sound data and most $P\rho T$ data within $\pm 0.01\%$ and $\pm 0.1\%$ in pressure, respectively.

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